

# Softwood – hardwood hybrid members and connections

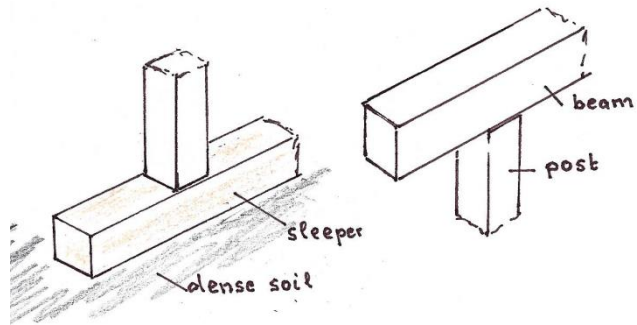
Ernst Gehri

Stockholm – 19.01.2018

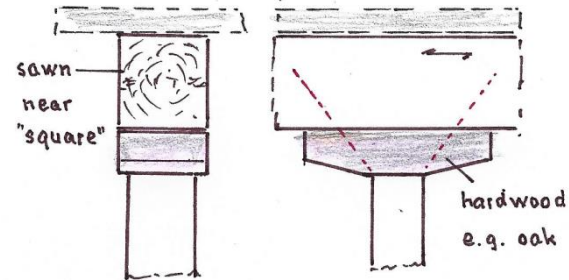
# softwood ↔ hardwood

Let's start with a very common situation

→ Introduction of a load perp. to grain in softwood



based on experience: use of hardwood sleeper or saddle

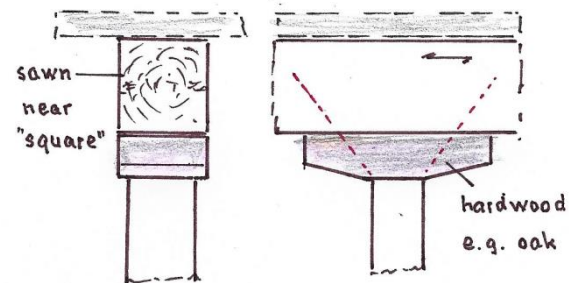
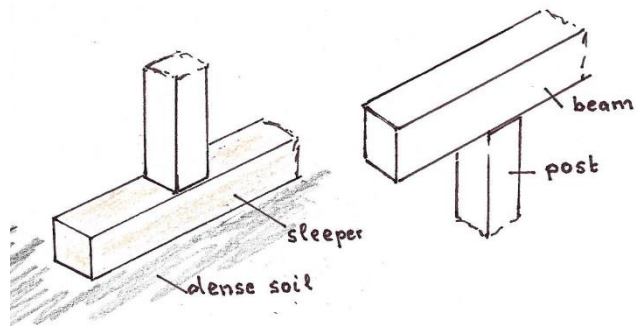


# softwood $\longleftrightarrow$ hardwood

Let's start with a very common situation

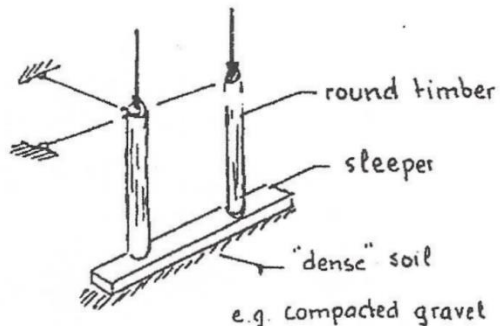
→ Introduction of a load perp. to grain in softwood

based on experience: use of hardwood sleeper or saddle



→ strength: compression perp. to grain (A. Föppl – 1904)

What is the bearing capacity? Which load should be assumed as safe or allowable?

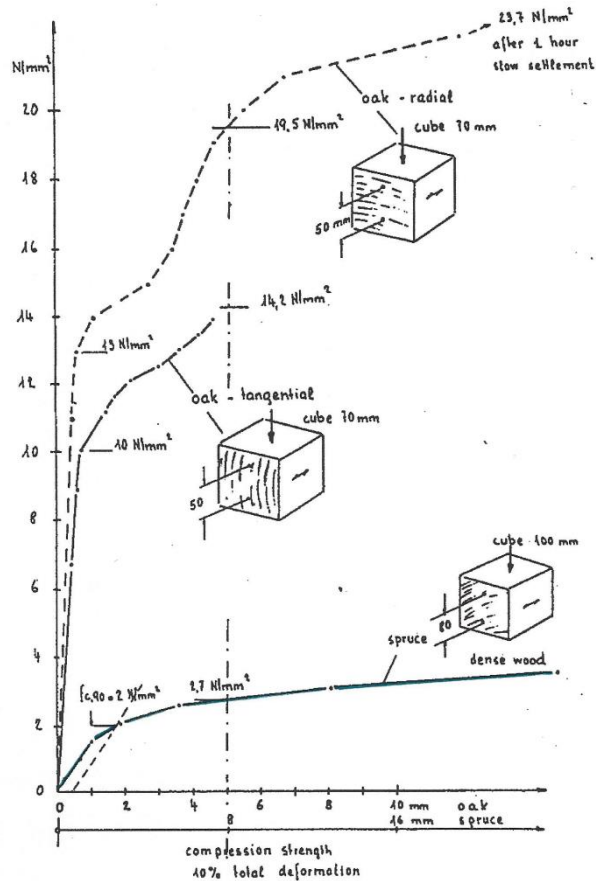


- material quality (e.g. function of species)
- material behaviour (deformation, failure)
- geometric conditions (e.g. partial loading)
- moisture content
- effect of time (creep)
- safety factors

Figure 1: Typical questions and factors which may influence the answer

## Here part of the answer's

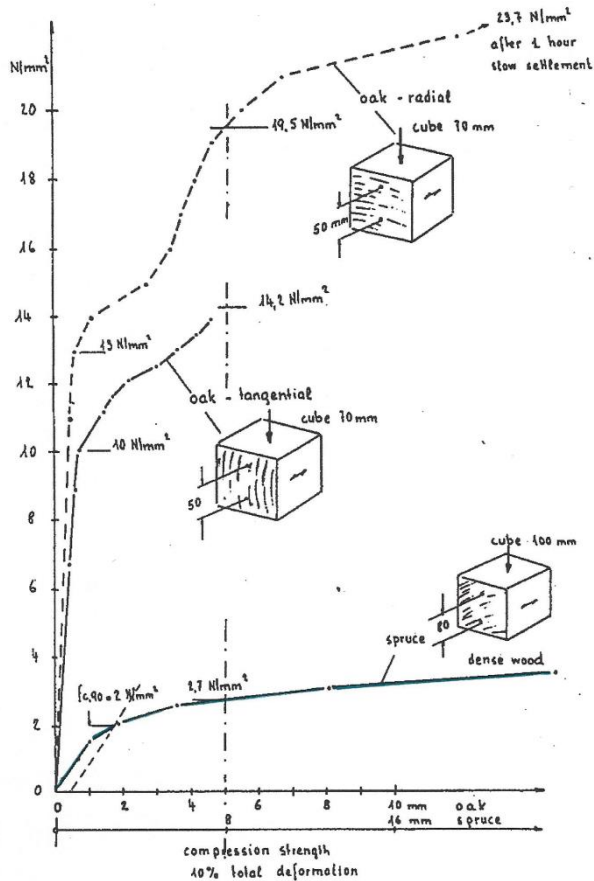
from A. Föppl (1904)



A.Föppl headed more than 100 years ago the «Mechanisch-Technisches Laboratorium» at the TU München. He was scientist and engineer: the specimens used corresponded to structural size

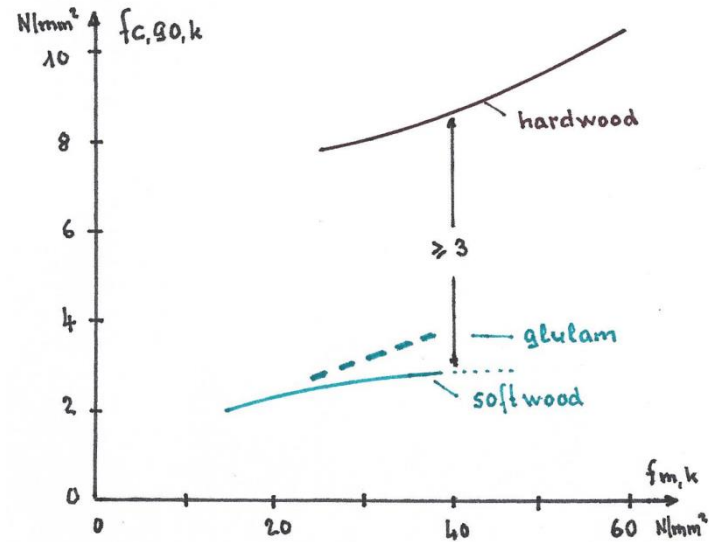
Here part of the answer's

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and where we are 100 years later

char. values for sawn wood and for glulam (only softwood!)



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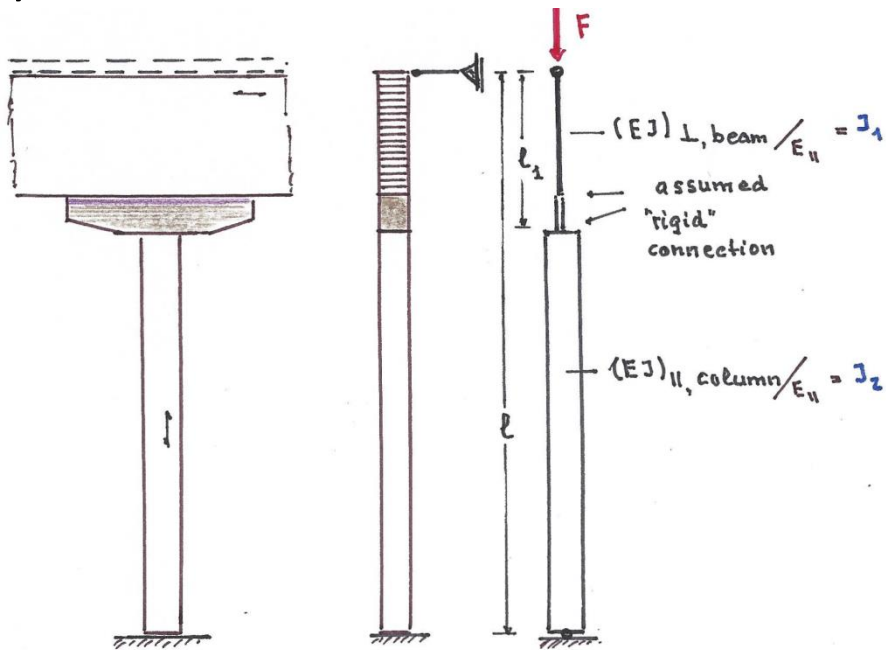
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# Use of glued-laminated beams: slender sections

**problem of instability**

higher concentrated forces

system

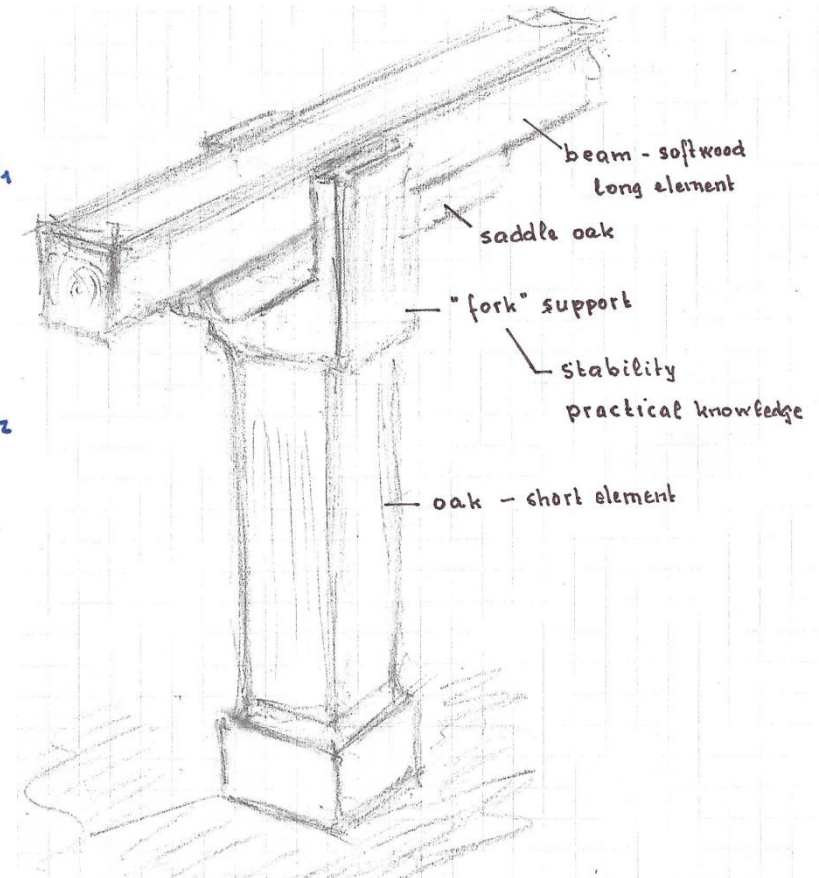
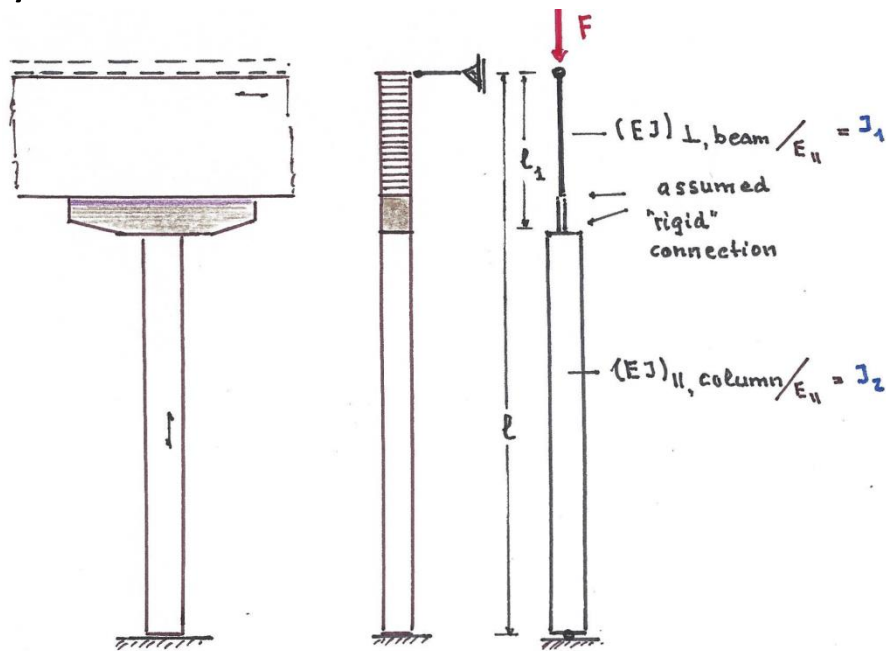


# Use of glued-laminated beams: slender sections

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## Possible solutions:

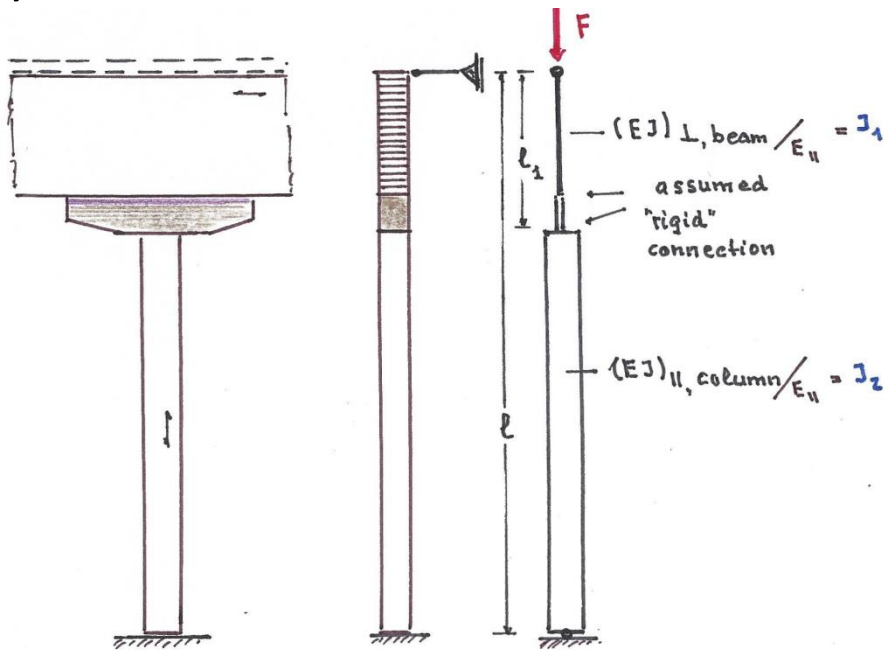
- by applying lateral holds (fork-like)  
often not accepted by architects

# Use of glued-laminated beams: slender sections

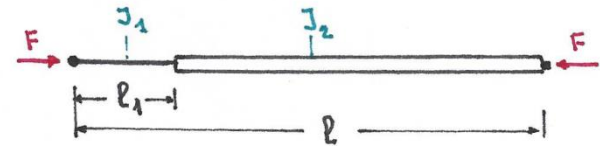
## problem of instability

higher concentrated forces

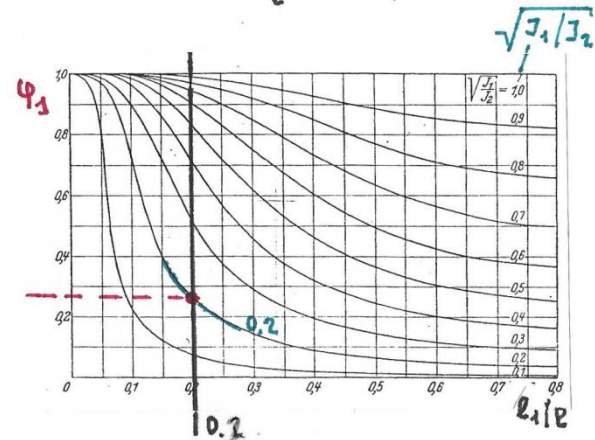
system



with  $l_1/l = 0,2$  and  $J_1/J_2 = 0,04$



$$F_{cr} = \psi_1 \cdot \frac{\pi^2 E J_2}{l^2} \quad \text{with } \psi_1$$



from A. Pflüger : 1950

## Possible solutions:

- by applying lateral holds (fork-like)  
often not accepted by architects
- by integrating hardwood saddle into beam (use of hardwood lamellae locally)

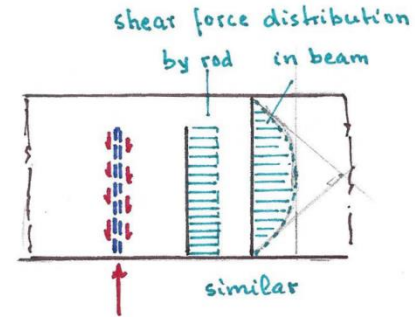
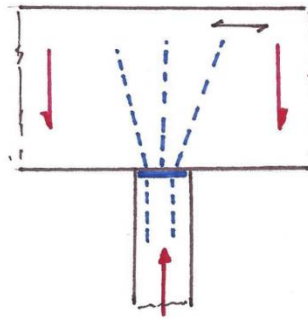
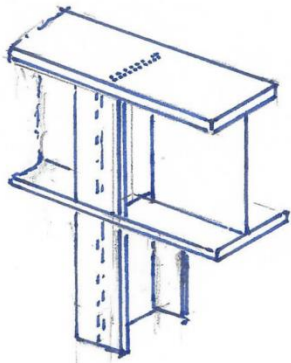


# Higher load introductions

point loads up to  $F_d = 1'000$  kN

too large contact areas (even with hardwood)

same solution as for steel beams



Advantages of load introduction by glued-in rods

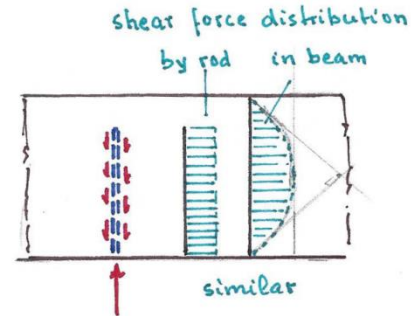
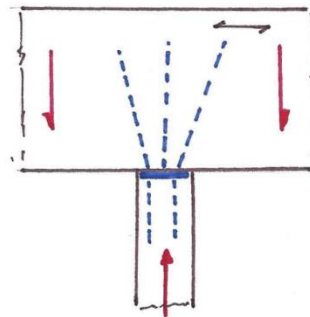
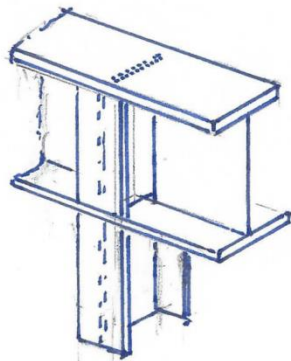
Possible to avoid saddle of hardwood

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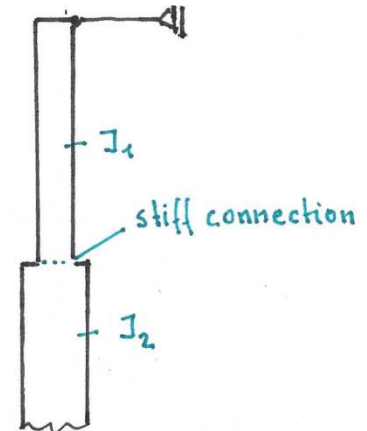
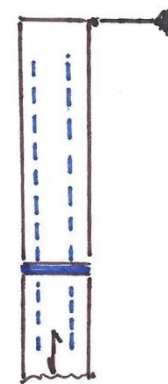
Possible to avoid saddle of hardwood

"column" integrated into beam

$$J_1 \approx 2/3 \text{ to } 3/4 \text{ of } J_2$$

$$\text{with } \sqrt{J_1/J_2} \approx 0.8$$

$$\text{and } l_1/l_2 \approx 0,2 \rightarrow \varphi_1 \text{ near } 1.0$$

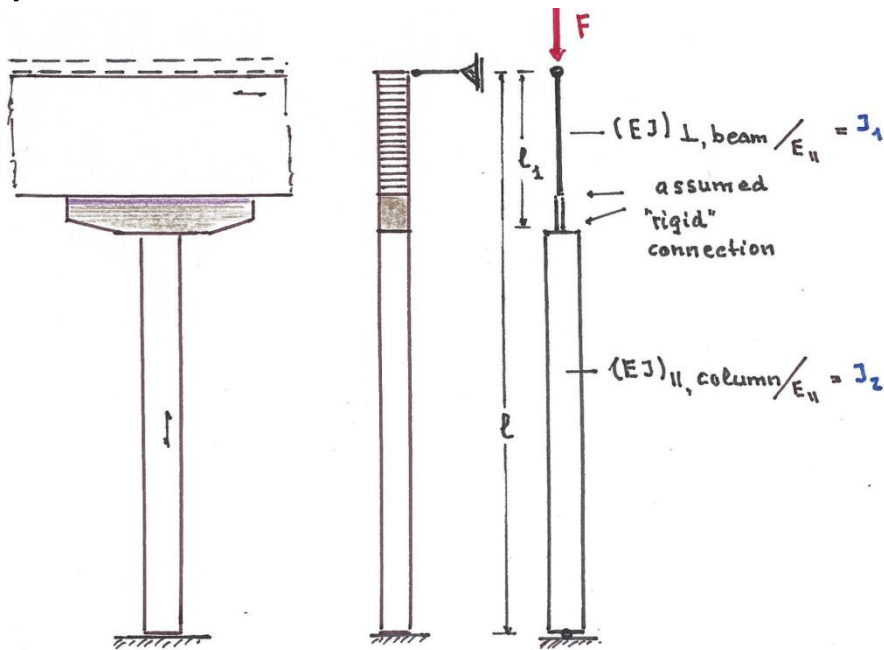


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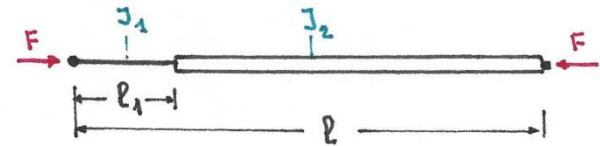
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higher concentrated forces

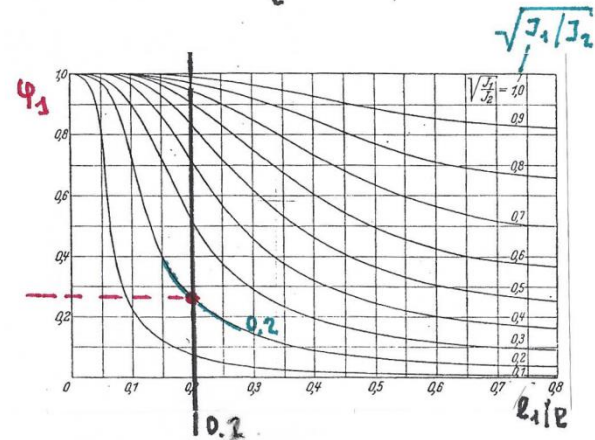
system



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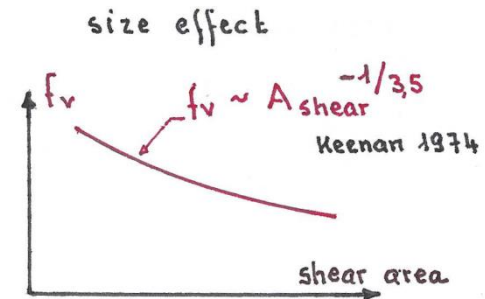
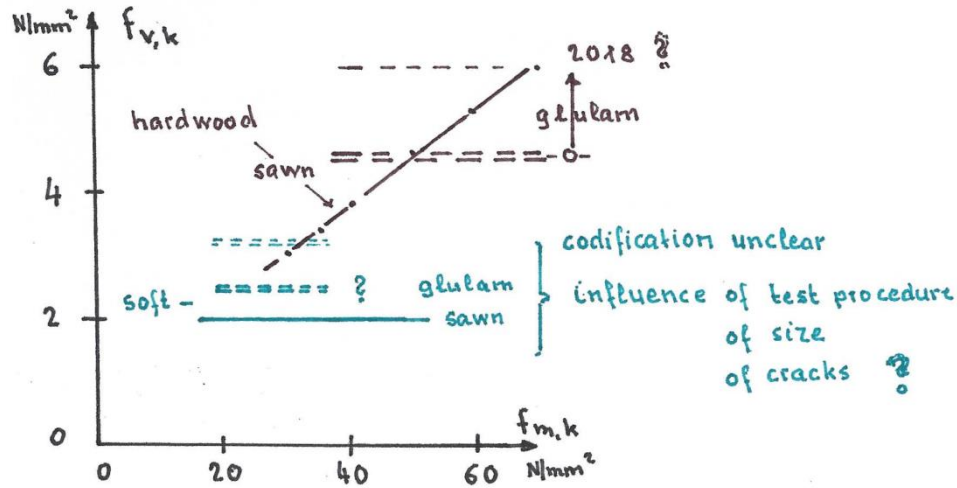
## Possible solutions:

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often not accepted by architects
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# Strength – on shear (parallel to grain)

## comparison softwood - hardwood

from EN's (glulam only softwood)



Problem: test procedure

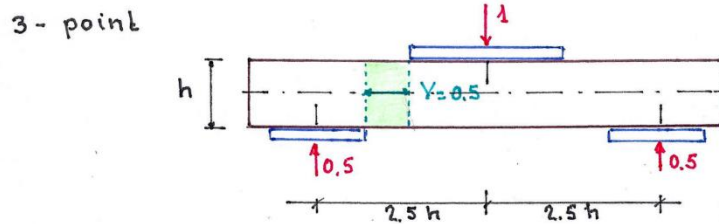
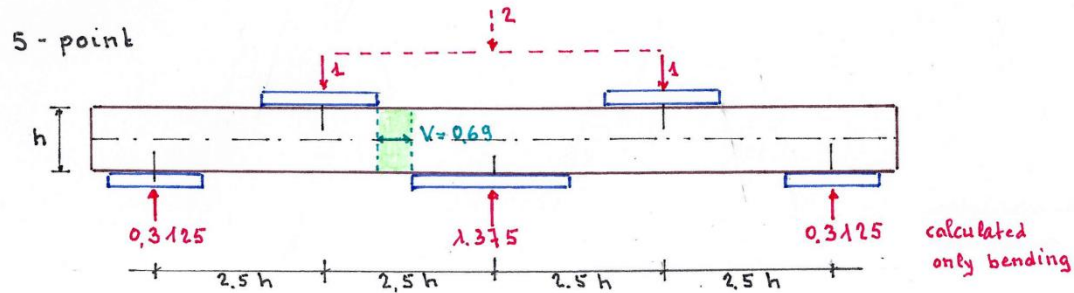
3-point / 5-point / type of load introduction / size of shear area

# Shear strength: test - procedures

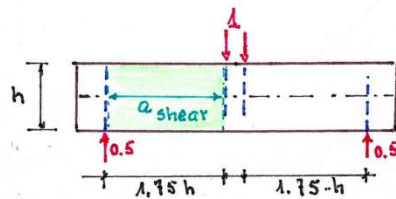
Note: 5-point was introduced to avoid

influence of drying cracks at beams end (often in lumber), but

no difference found (same relationship for wet and dry wood!)



with glued-in rods

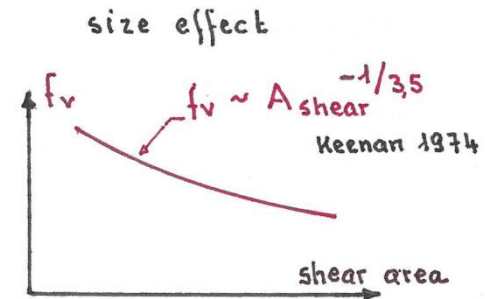
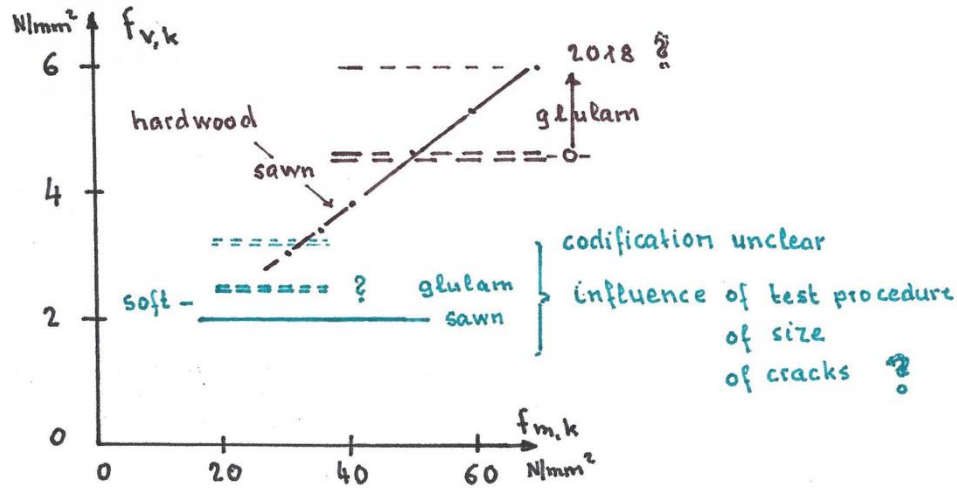


Note: higher strength values obtained 5-point than 3-point, due to smaller effective shear area

# Strength – on shear (parallel to grain)

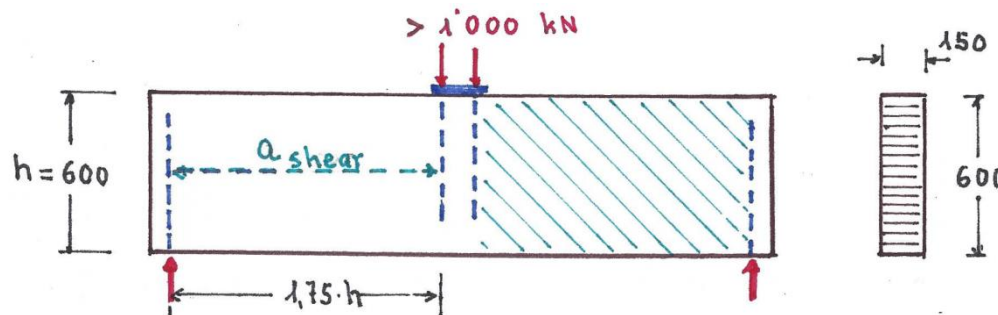
## comparison softwood - hardwood

from EN's (glulam only softwood)



Problem: test procedure

3-point / 5-point / type of load introduction / size of shear area



tests: beech glulam  
 $f_{v,05} \approx 6$  to  $8$  N/mm<sup>2</sup>

## shear test on larger sections (glulam spruce and hardwoods)

shear test on **glulam beech 120/600**

Limited by capacity of testing rig:

$$2 \cdot V = 900 \text{ kN}$$

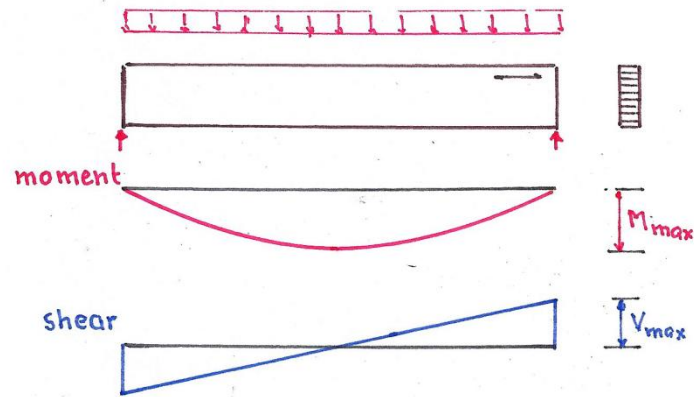
with measurement of shear modulus

shear test on **glulam spruce 140 / 1'000**



# How to optimize the classical glulam beam?

→ use better specific properties of timber species



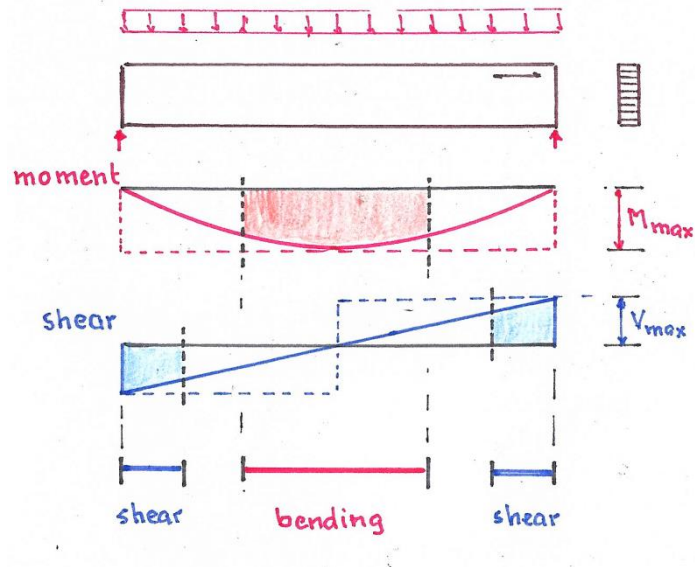
classical glulam beam

constant, prismatic, rectangular sections



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classical glulam beam

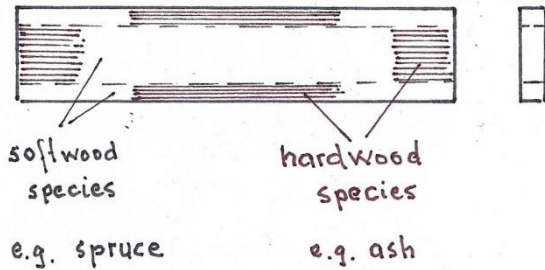
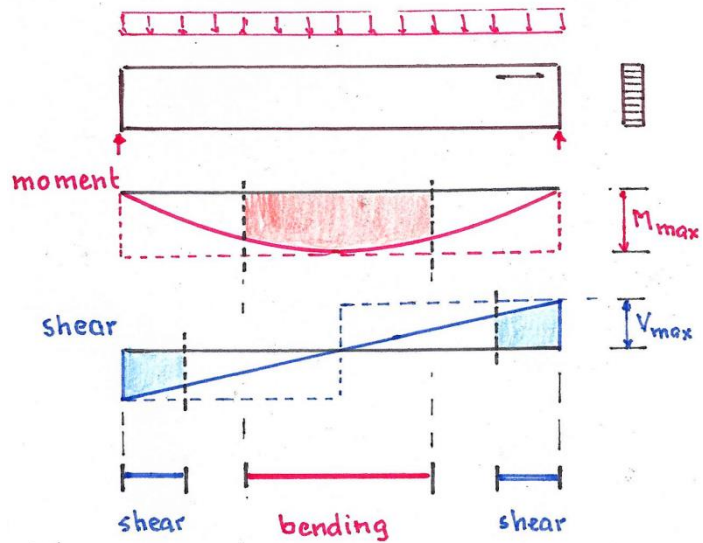
constant, prismatic, rectangular sections

same resistance - **bending / shear** – over length

**not needed !**

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classical glulam beam

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same resistance - **bending / shear** – over length

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from **actual** fabrication requirements:

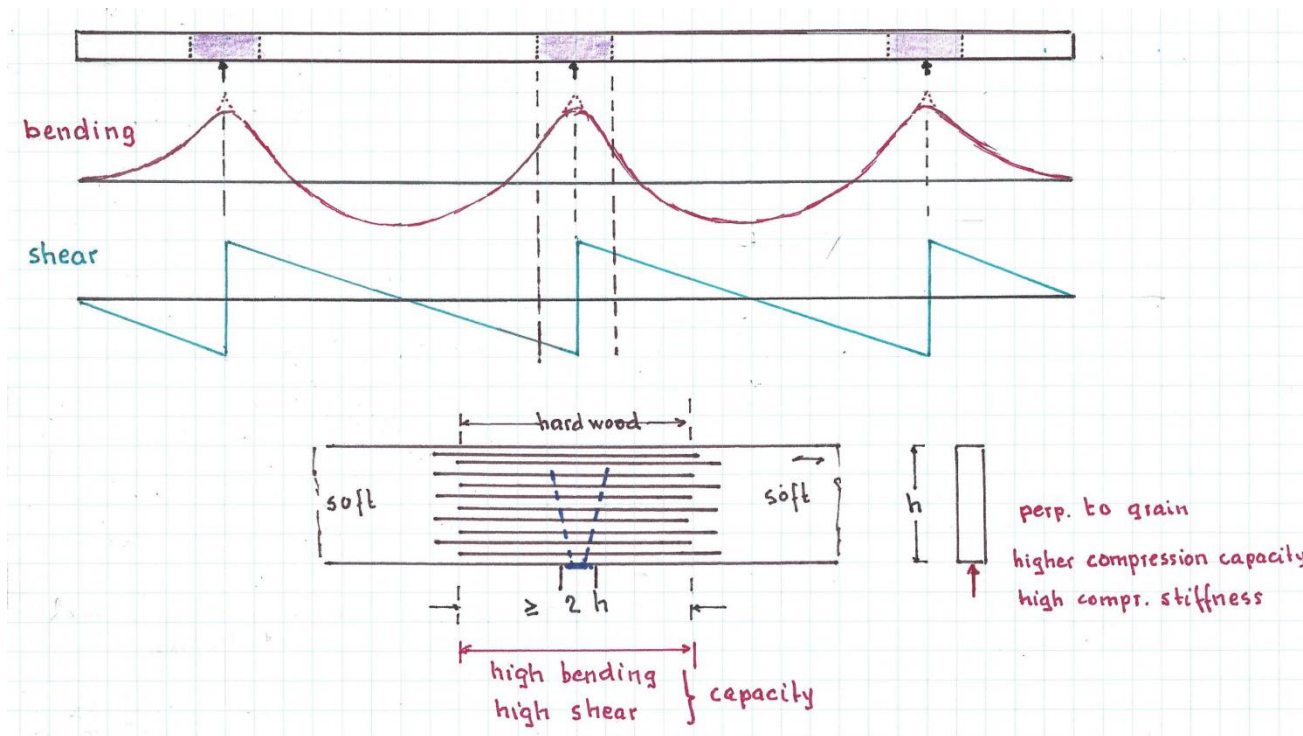


use same glue-laminating procedure

## actual properties of hardwood glulam

bending strength	$f_{m,k}$	= 48 N/mm <sup>2</sup>
shear strength	$f_{v,k}$	= 6 N/mm <sup>2</sup>
compression strength	$f_{c,90,k}$	= 8 N/mm <sup>2</sup>

**Continuous beams:** Use only in high stressed zones (e.g. over supports)



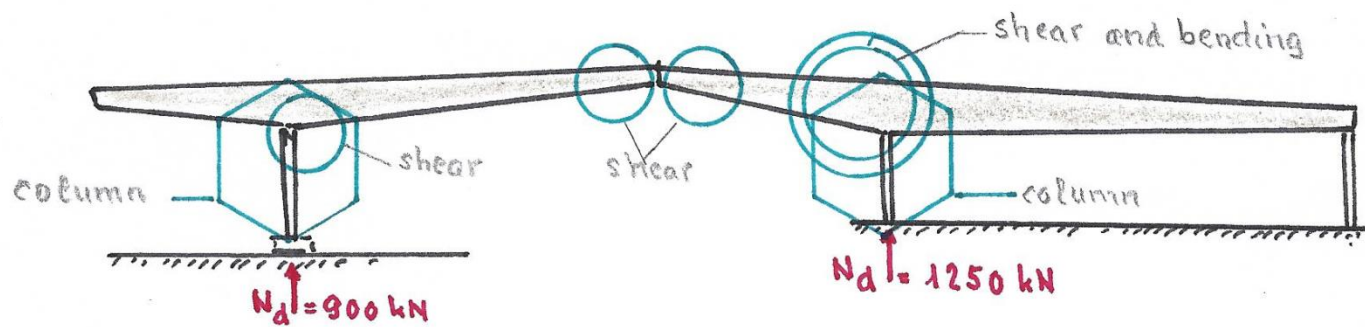
Preferably ash → (same lamella thickness as spruce = 40 mm)

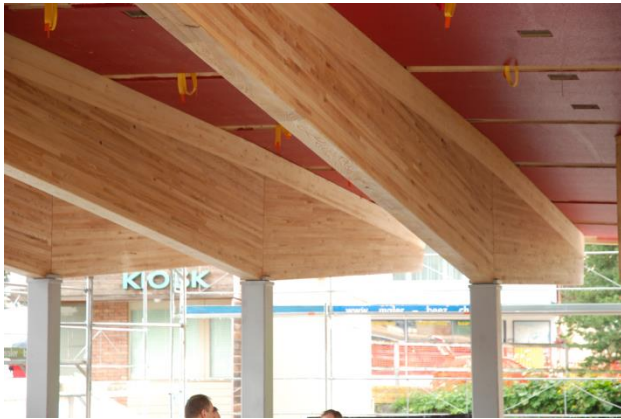
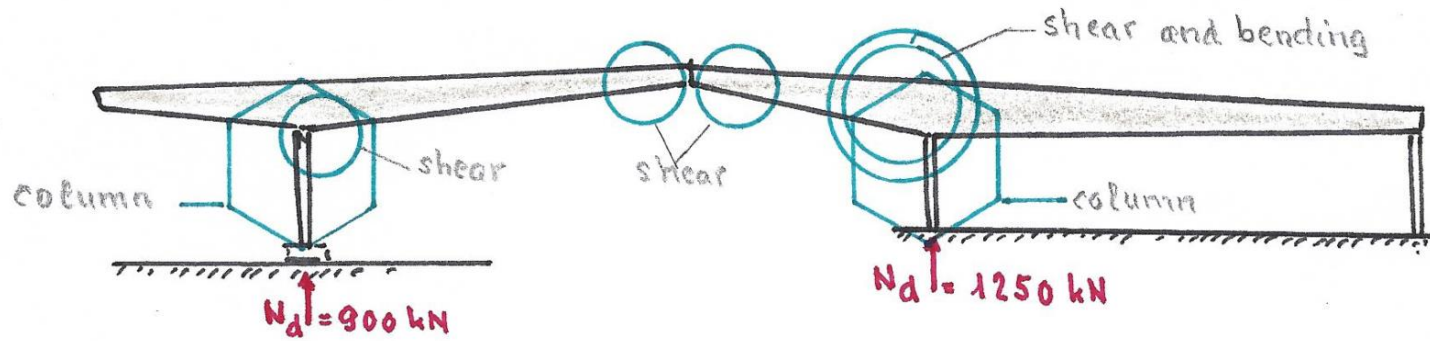
Finger-joint: no problem to achieve softwood data ( $f_{t,j,k}$  up to 33 N/mm<sup>2</sup>)

## Hybrid beams (lengthwise) spruce/ash

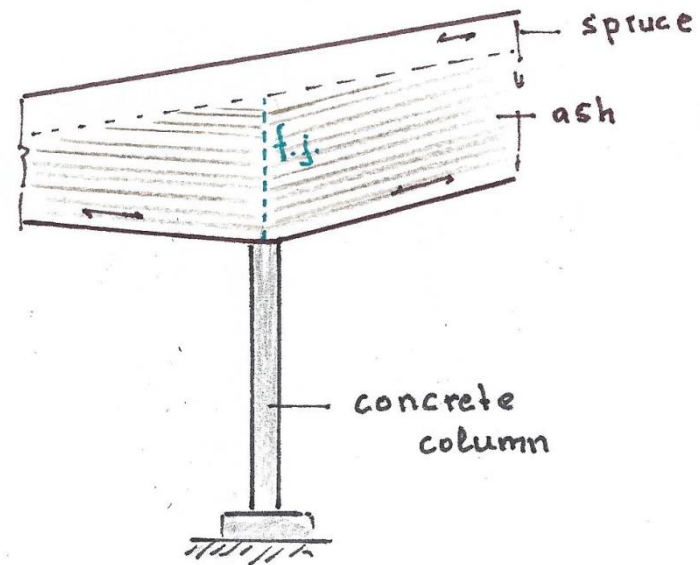


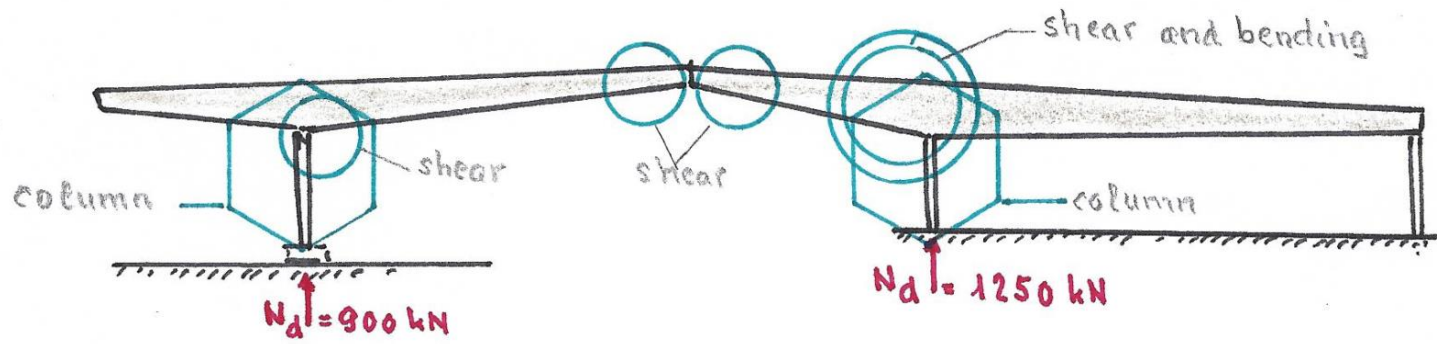
# Case Arosa: hybrid beams ash / spruce



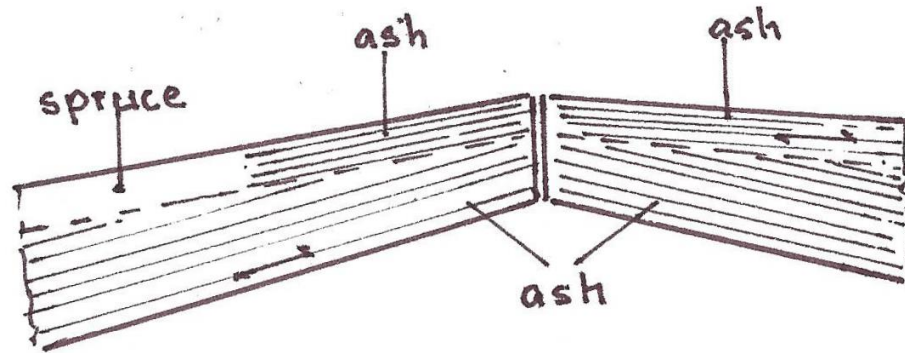


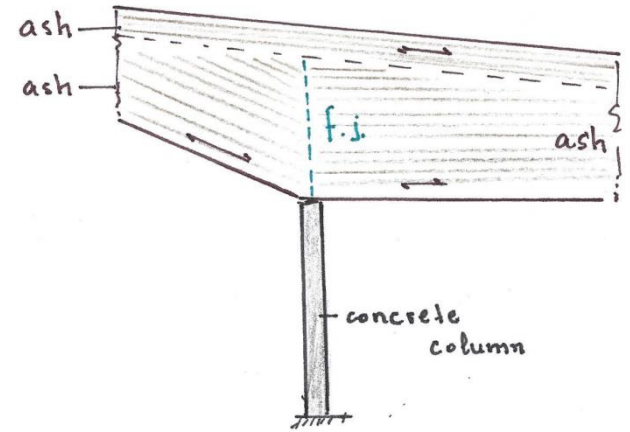
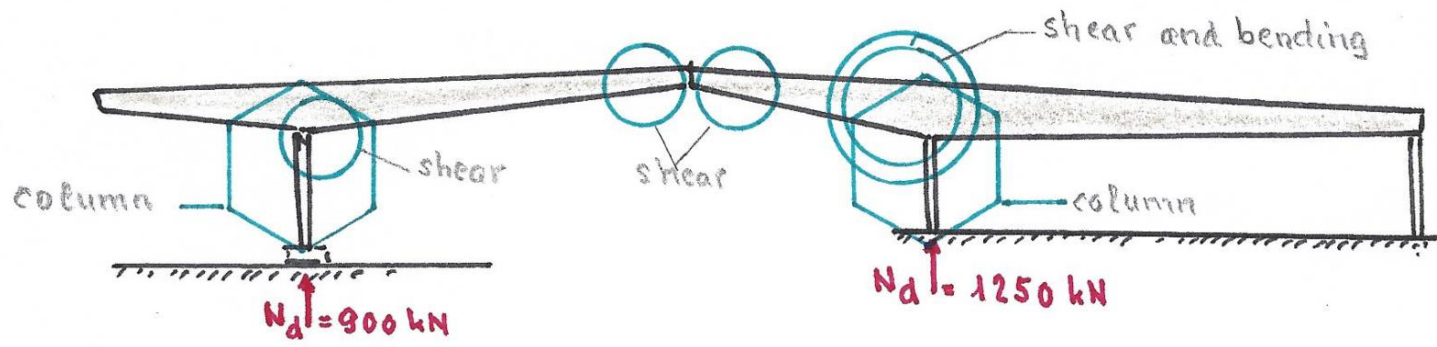
- load introduction column/beam → ash + glued-in rod
- shear force → ash
- free standing column → glued-in rod





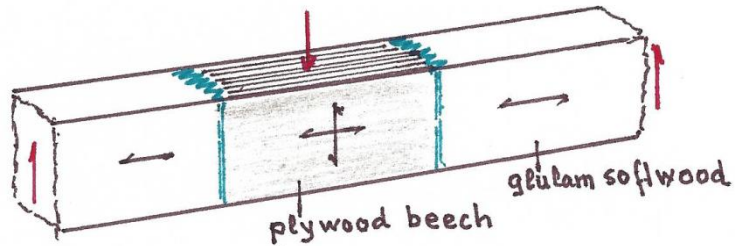
shear force → ash







# glulam softwood / plywood beech

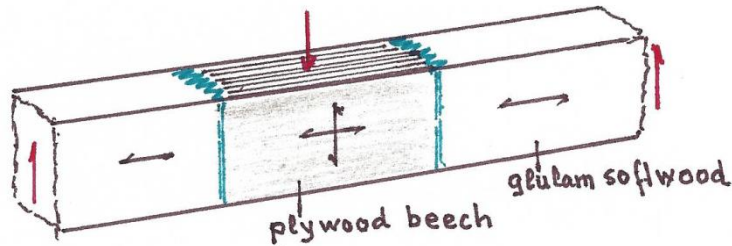


finger-joint resistance governed by softwood  
**bending capacity** taken as  $0,8 \cdot f_{m,k,spruce}$

!



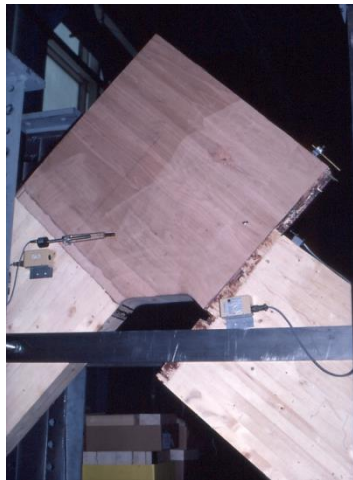
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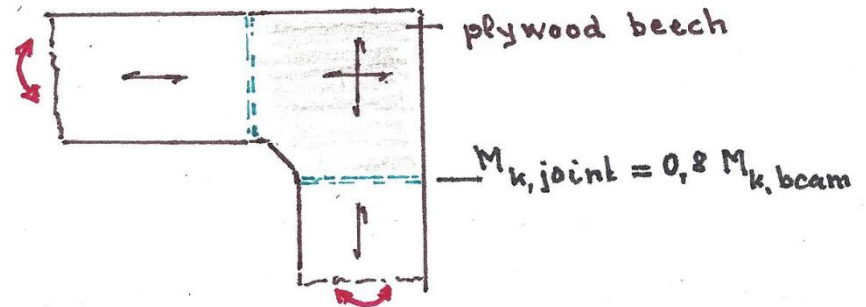
→ important: **higher shear capacity**

→ e.g. use as **frame corner**



simple design

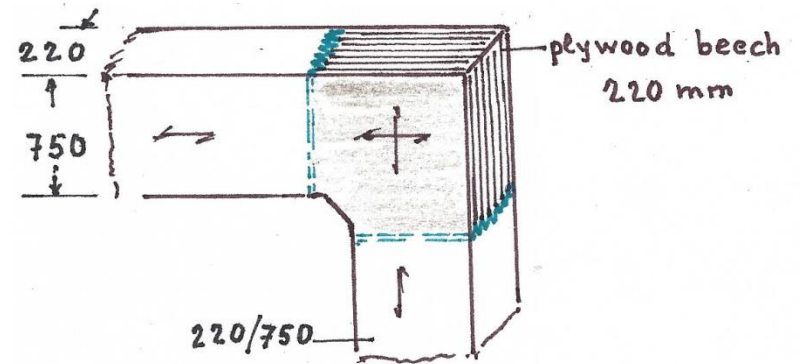
only control of  
finger-joint capacity!



## Case: bridge Eggiwil (1982)

2-lanes bridge

### Portal frame



plywood beech: thickness 220 mm  
outside veneer: spruce (esthetic)



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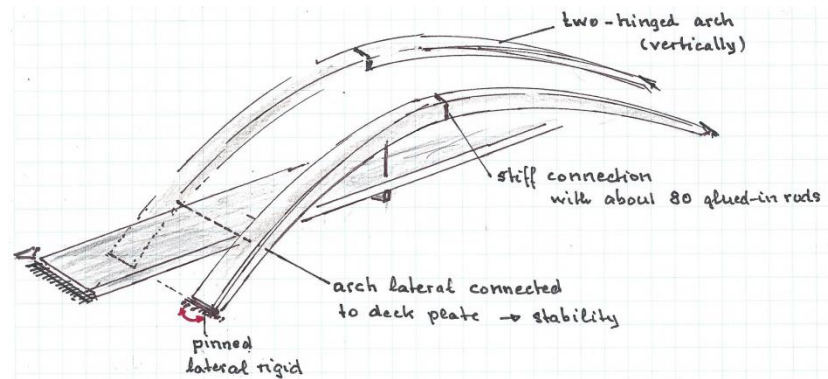
plywood configuration adapted to  
geometry of finger-joint-cutter



## Case: bridge San Nicl  (1993)

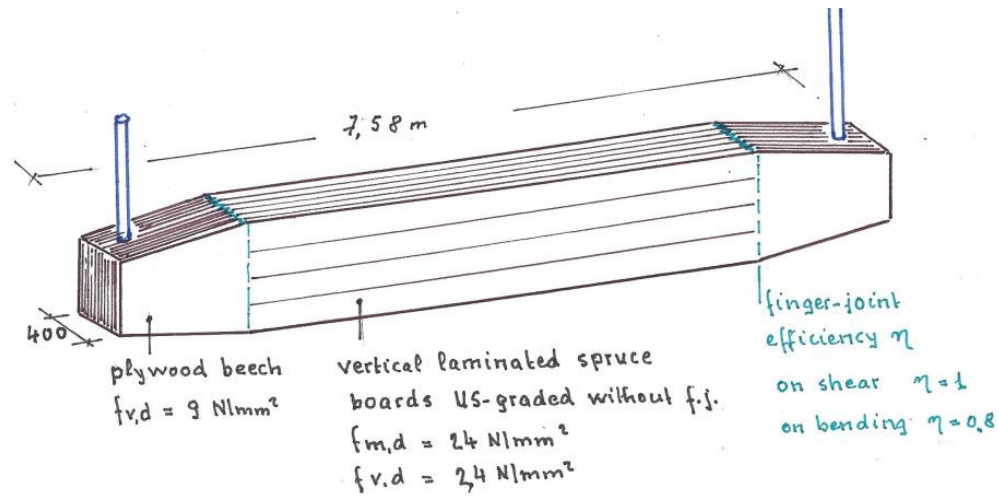


static system:

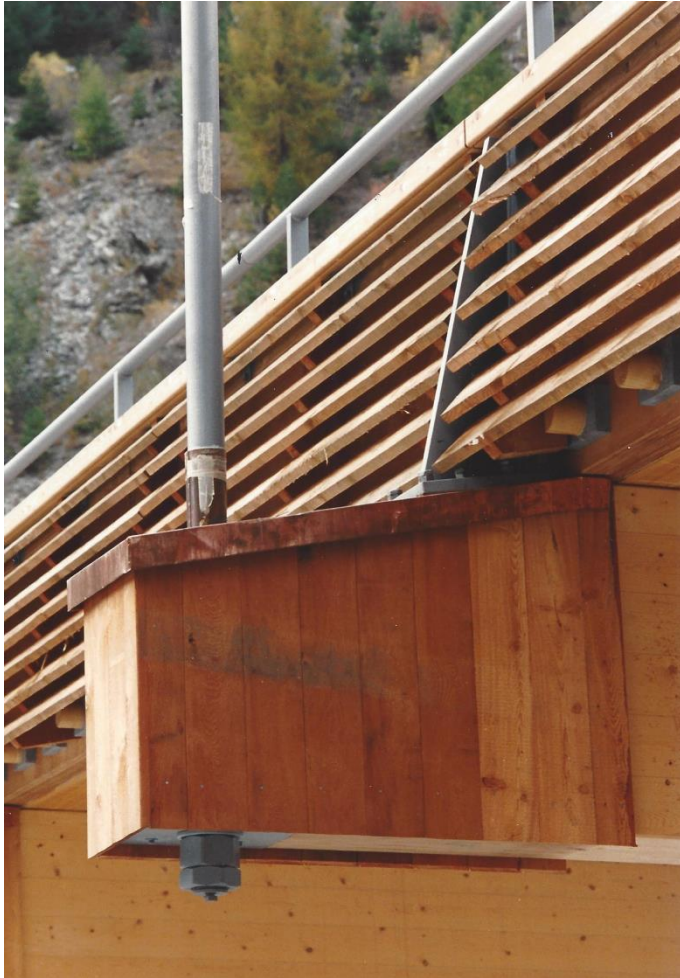


**Cross-beam:** vertically glued-laminated spruce (without finger-joints)  
ends in plywood beech finger-jointed

Dimensions:



**Cross-beam:** vertically glued-laminated spruce + ends in plywood beech finger-jointed



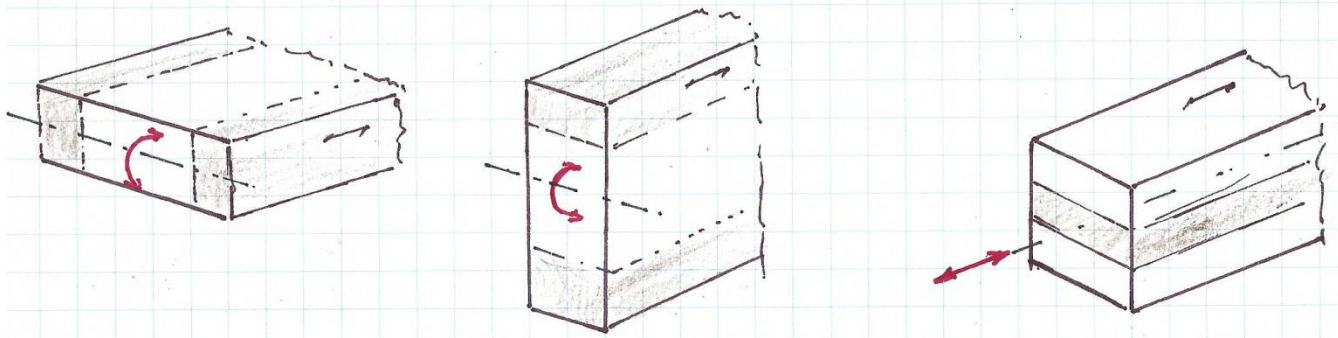
natural protection of plywood beech by encasement

finger-joint plywood / softwood glulam  
section 400 x 885 mm



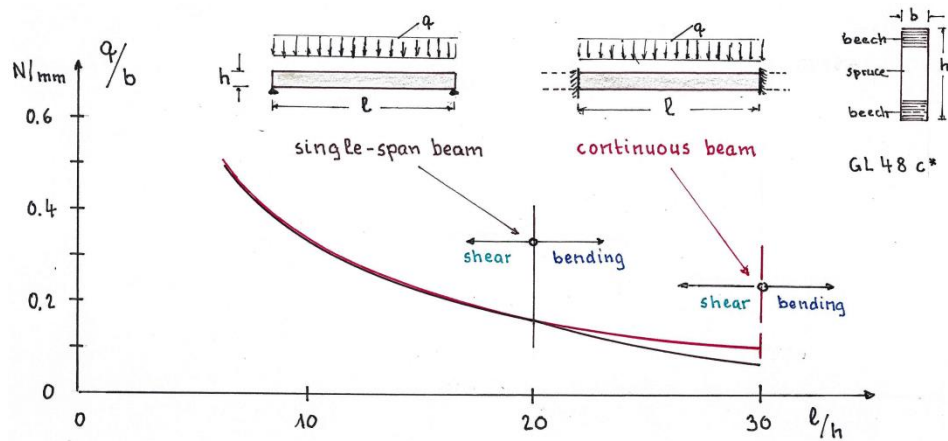
# composite elements - softwood + hardwood

## classical hybrid beam



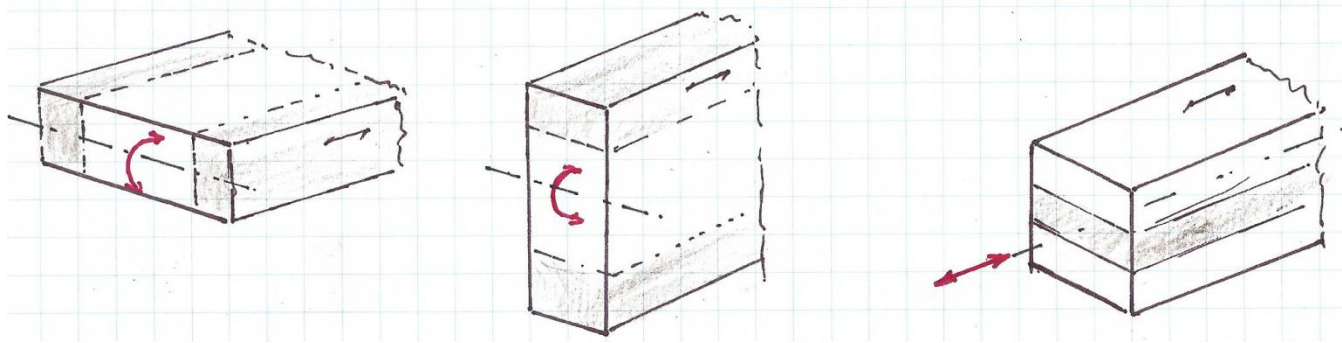
higher bending strength + stiffness

attention: low shear capacity





# composite elements - softwood + hardwood



bridge decks prestressed

edge element: **perp. to grain** → hardwood

sawn / glulam / LVL / plywood

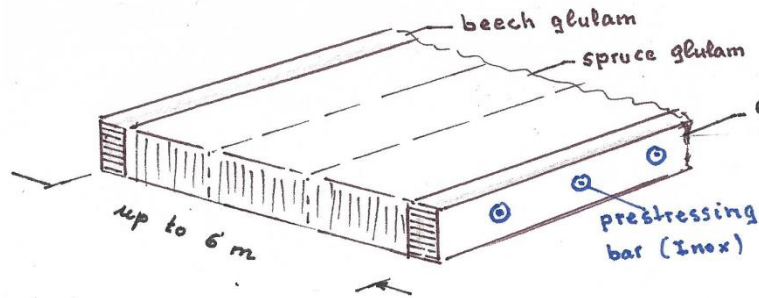
for chord of trusses

higher **rolling shear strength**

needed at node area



## Sins: Deck plate glulam spruce / glulam beech ( ≈ 70 m long )



- higher stiffness and strengt on bending and compression perp. to grain
- smaller contact plate (aluminum)
- less loss due to creep



# Connections

High performing hybrid elements → need of performant connections

## **dowelled connections**

- Most used in softwood-glulam limited to  $\eta \leq 0,65$  (due to reduction of section)
- Actual (EYM) design rules lead to brittle behaviour !
- **Need for design rules specific for hardwood** (and high ductility  $D = w_u/w_y > 5$ )

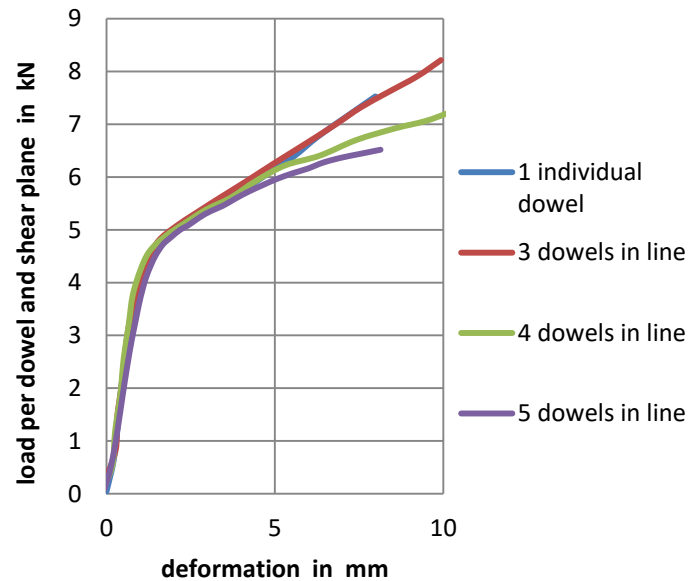
# Dowelled connection

- for ductile behaviour → high slenderness of dowel  
→ sufficient distances  $a_1$
- no group effect! → independent of  $n$  →  $k_{red} = n^0 = 1$

test with LVL-beech:



beech GL48 - dowelled connection  
of high ductility



performance max.  $\approx 30 \text{ N/mm}^2$  (based on full section)

# Connections

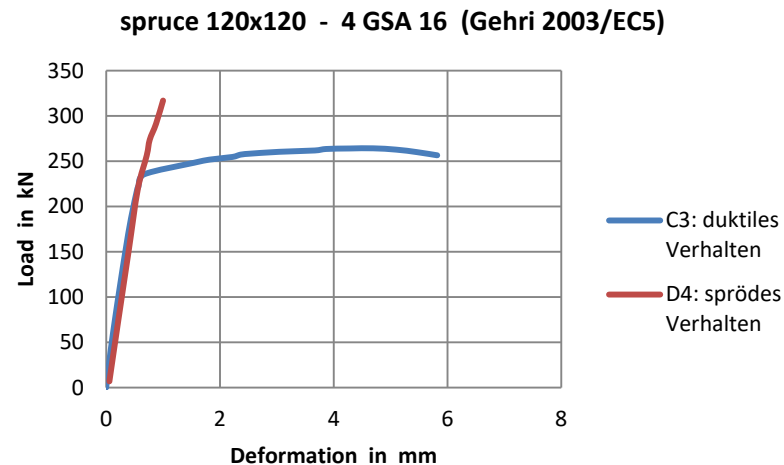
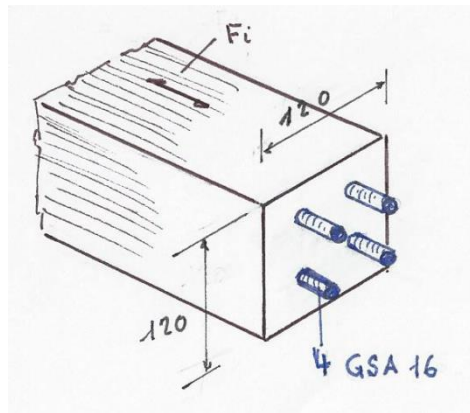
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## glued-in rods

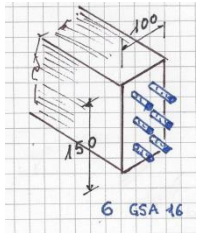
- Technology: same as for softwood glulam
- Criteria: behaviour is governed by the steel (strength and ductility)  
all other (brittle) failure modes are excluded (Gehri/1996)



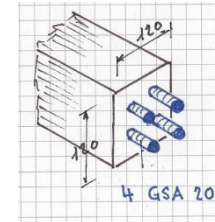
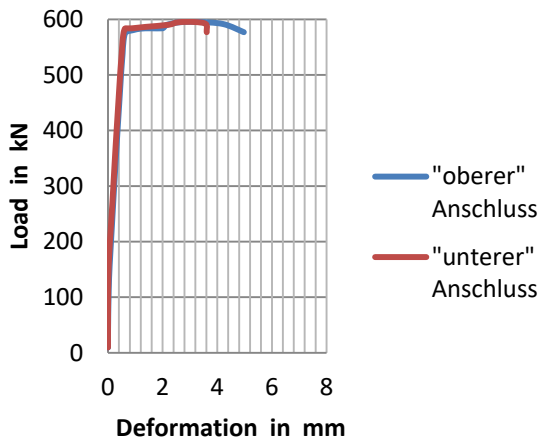
# Tests of glued-in rods with LVL beech

## GSA-system glued-in rods

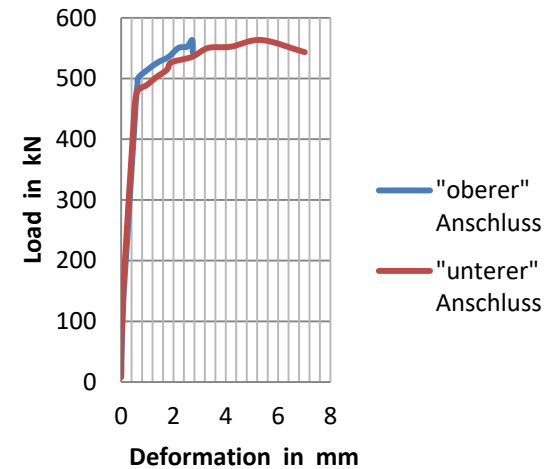
ductile behaviour    no group effect !



GSA 16.8 - 52.1 – group of 6



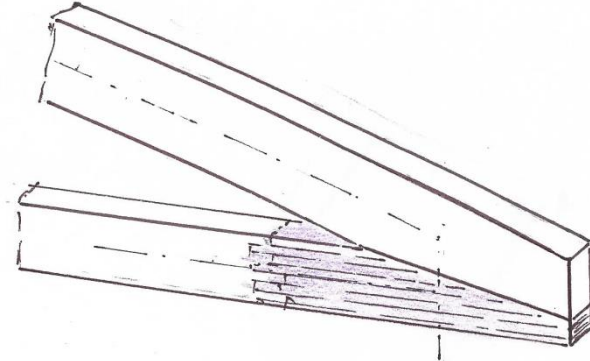
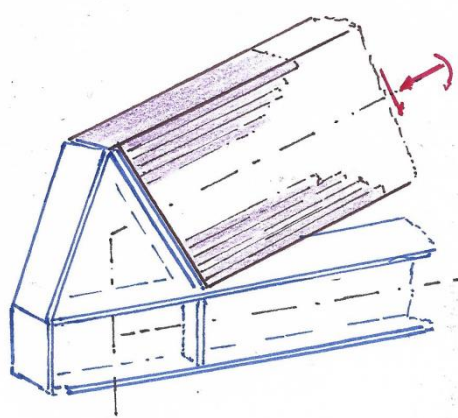
GSA 20.8 - 46.1 - group of 4



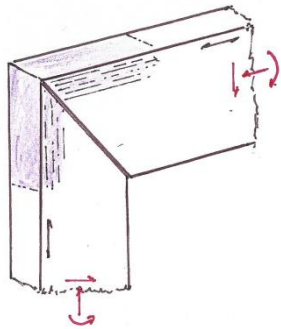
$$f_{t,0,brutto} \approx 40 \text{ N/mm}^2$$

with optimized configuration

# Connections with hardwood inserts and glued-in rods



# EIZ – Frutigen 2005

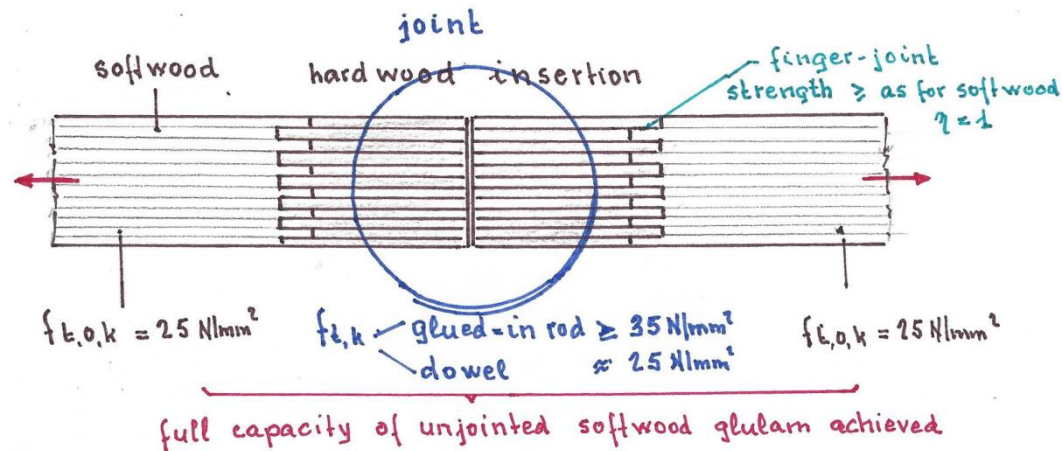




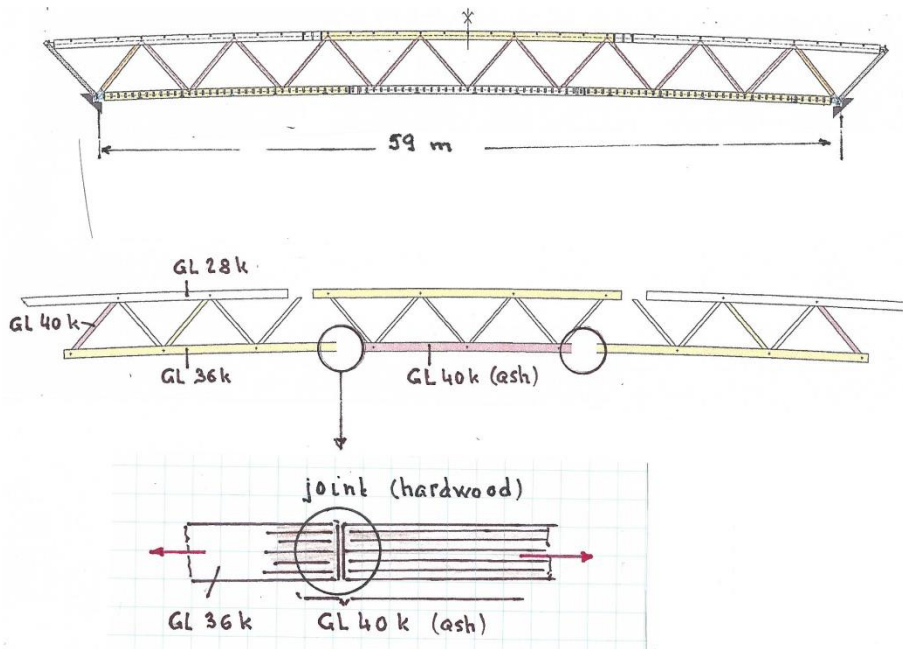
## Local inserts of hardwood (glulam/plywood)

- Use higher performance of connectors (dowels / glued-in rods) in hardwood
- **Avoid reduction in softwood members**

With glulam insert: **joint performance  $\eta = 1$**  (for softwood members)



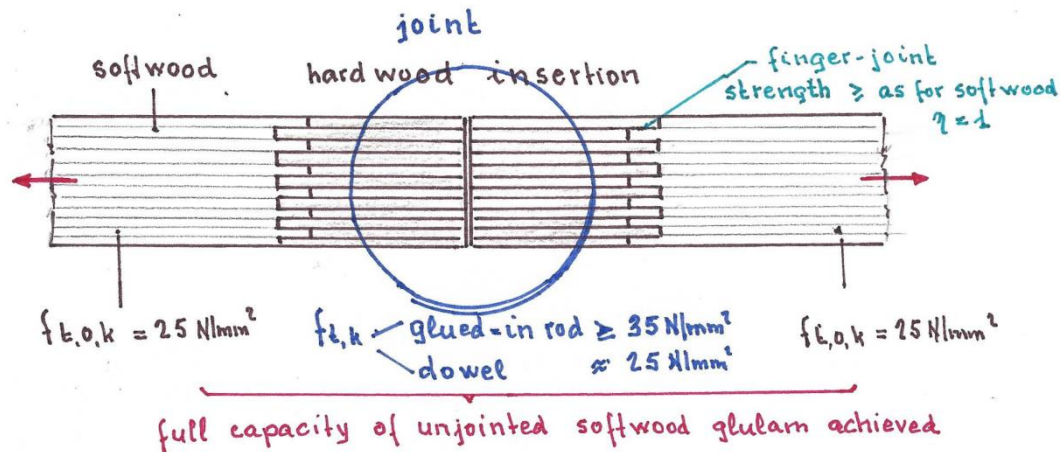
# Neumatt bridge – truss system – glulam spruce / ash



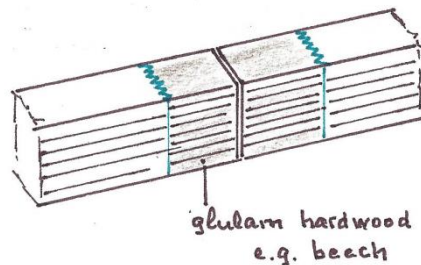
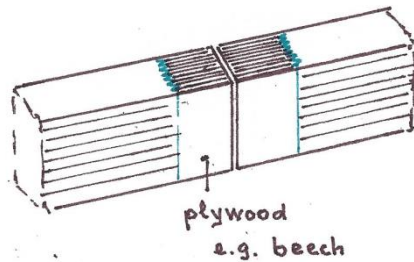
## Local inserts of hardwood (glulam/plywood)

- Use higher performance of connectors (dowels / glued-in rods) in hardwood
- Avoid reduction in softwood members

With glulam insert: joint performance  $\eta = 1$



With plywood insert: **joint performance  $\eta = 0,8$**

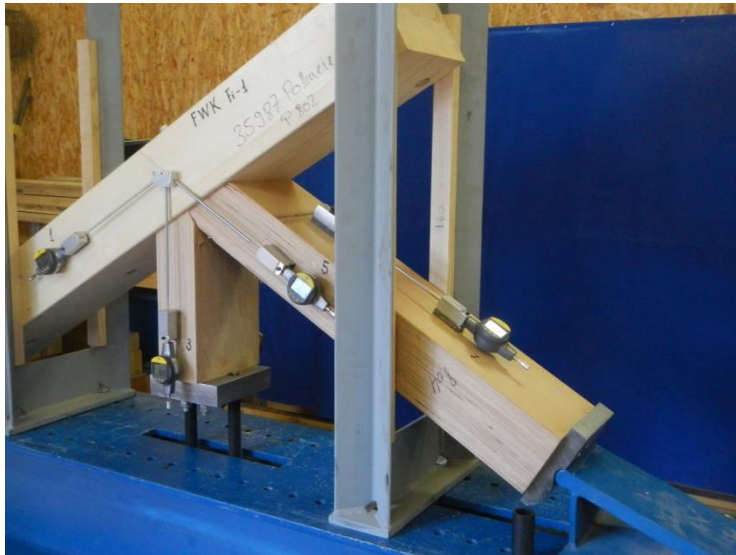
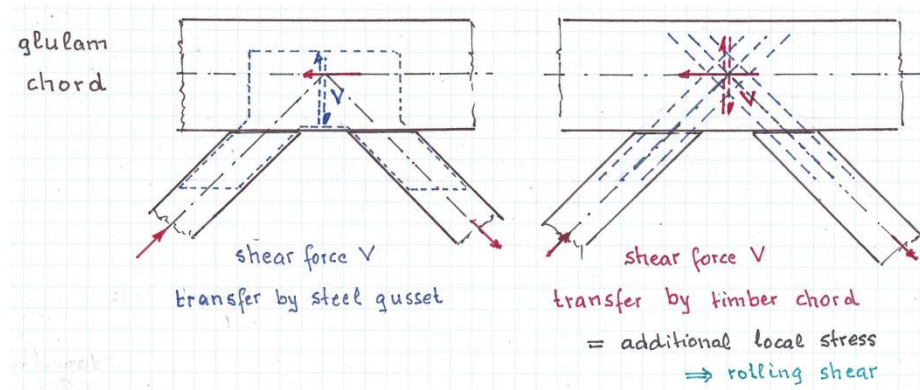


finger-joint over full section

# Typical situation in parallel chord trusses

→ transfer of diagonal forces in chord

Connected :      with dowels      with glued-in rods



## Use – as possible – more appropriate systems



→ **fishbelly girder**

(here for a footway:  
exposition at n'H 2009)

Upper chord: **glulam ash**  
Diagonals: **sawn lumber ash**  
Lower chord: **LVL ash**  
End nodes: **plywood beech**

Connections: diagonals **screwed**  
End nodes: **finger-joint/glued-in rods**



**and remember**

August Föppl (1854-1924) : scientist and engineer

Experiments should be done under realistic conditions  
material and size



**Good luck !**